

Comparative Study Using Some Advanced Simulation Methods for Leaching of Cementitious Materials Over Ten Thousands of Years

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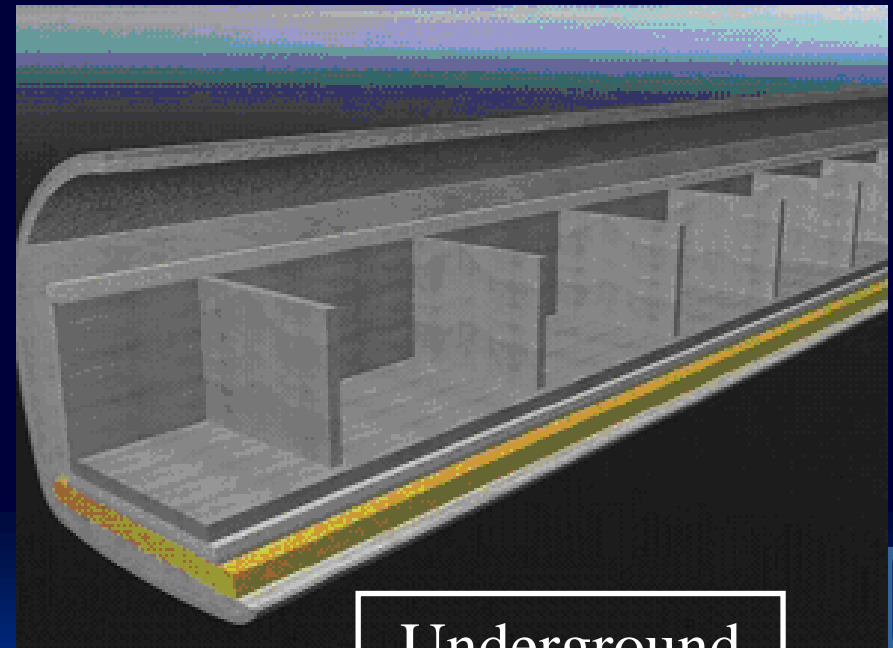


Nuclear power generation covers 30 percents of power generation in Japan.

Method for disposing radioactive waste is very important.

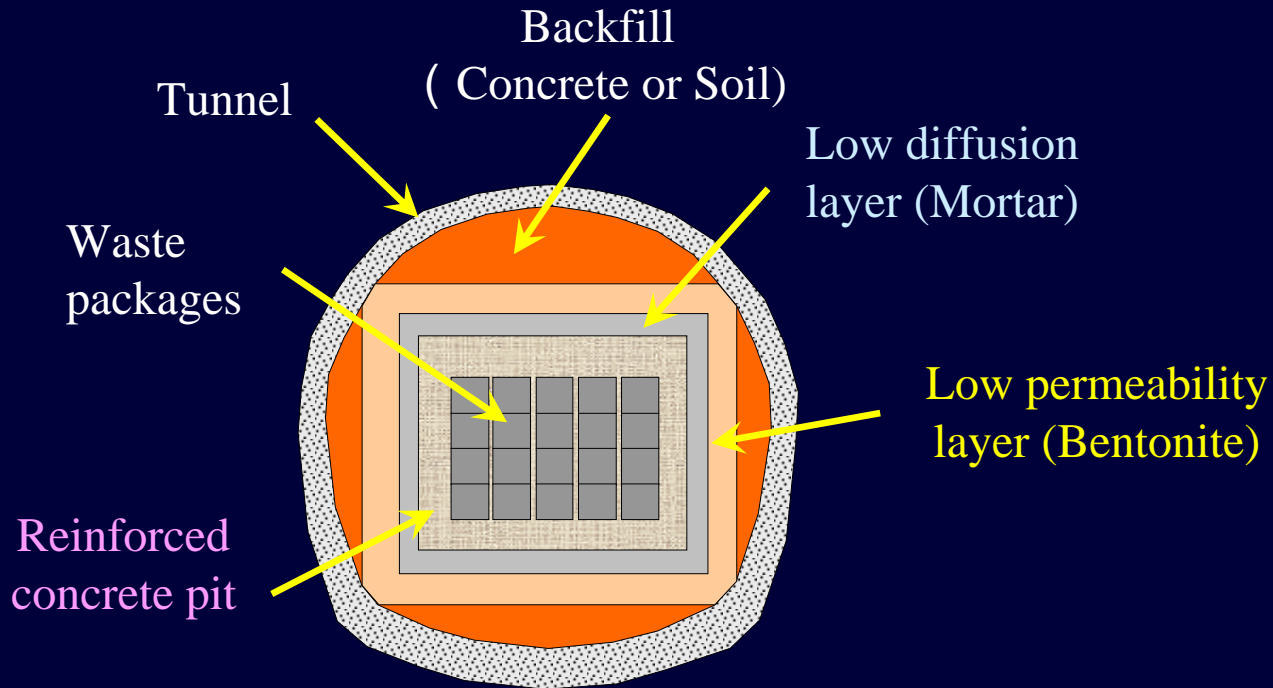
RADIOACTIVE WASTE

- High-level radioactive waste
 - Geological disposal
(~-300m)
- Low-level radioactive waste
 - Concrete Pit
(-10 ~ -5m)
 - **Sub-surface Disposal**
(-100 ~ -50m)



Underground
(-100 ~ -50m)

Cross sectional view of sub-surface disposal repository



Concrete pit : Maintaining stability of the repository

Mortar : Preventing radioactive nuclides to leak

Bentonite : Preventing underground water to permeate to the repository

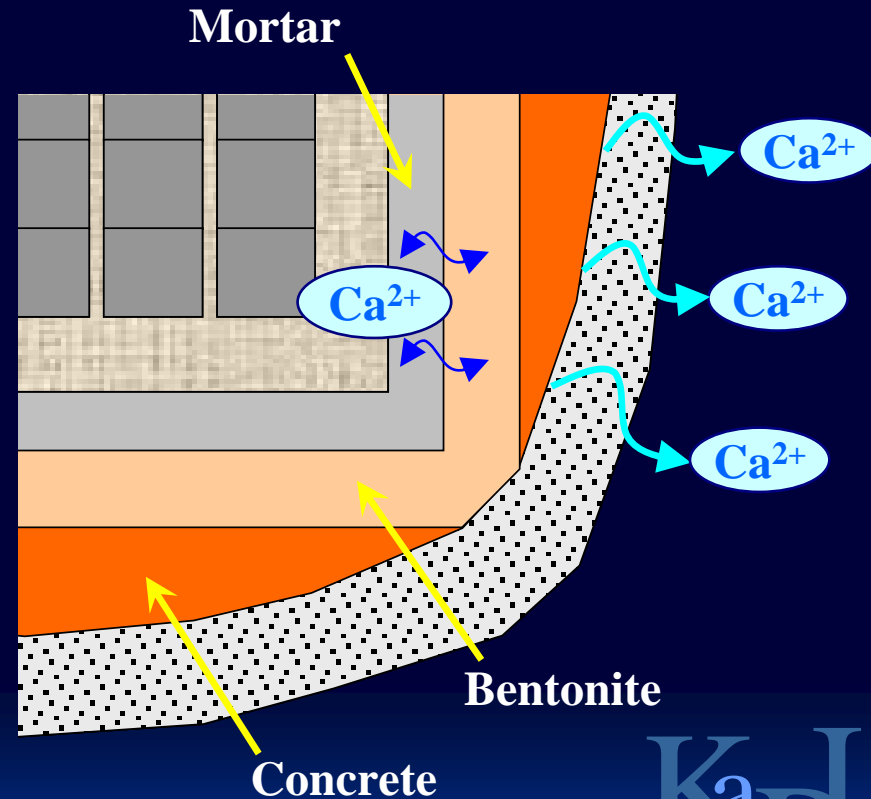
Long-term durability (over 10,000 years) is demanded for this repository

Evaluating long-term durability of concrete is necessary

Issues for cementitious material

- *Crack
- *Chemical degradation

- *Calcium leaching to underground water
- *Chemical reaction between mortar and bentonite



Simulation-code for evaluating calcium leaching

for example...

DuCOM, LIFE D.N.A., CCT-P

※Method of simulation is different.

Evaluating calcium leaching of
cement hydrates by 3 codes.

- What kind of deterioration will occur in sub-surface disposal repository?
- How fast is the deterioration speed?

Numerical Simulations

Dissolution/Precipitation of Hydrates

- ◆ Thermodynamic database
- ◆ Solid-liquid equilibrium for calcium

&

Mass Transfer

- ◆ Advection
- ◆ Diffusion
- ◆ Electrical potential

Experimental Models

$$L = a \times t^{1/n}$$

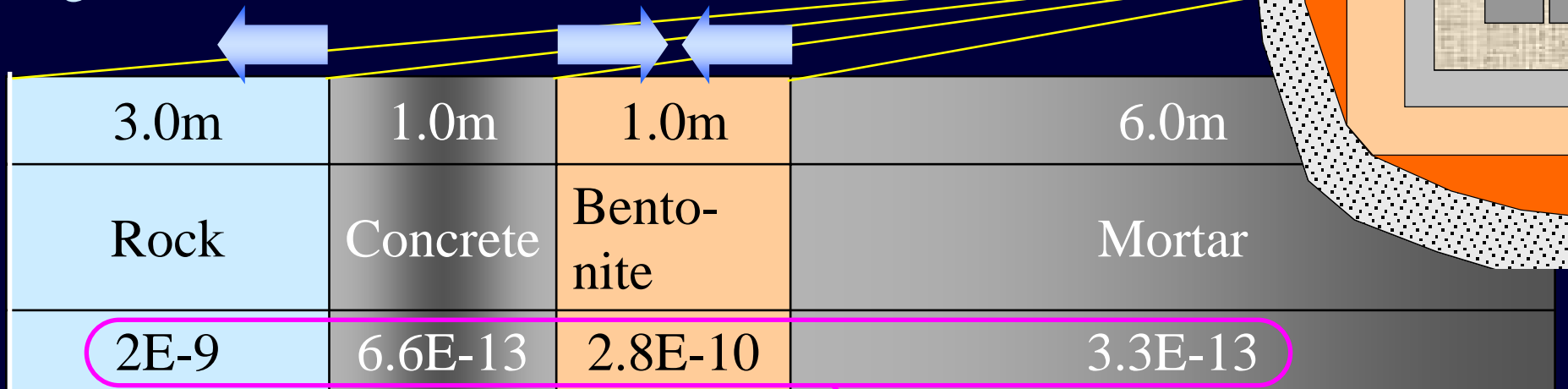
n ; parameter (generally n=2)
a ; constant parameter

Comparison of 3 codes

Code	Model of diffusion coefficient	Chemical reactions	
		Cementitious material	Bentonite
DuCOM	$D_{eff} = \frac{\phi \cdot S}{\Omega} \cdot \delta \cdot D_{ion}$	* Solid/liquid equilibrium for calcium	Absorption of Ca ions
LIFE D.N.A.	$D_{eff}^i = \eta \cdot \beta \cdot f(\phi) \cdot D_0^i$	* Solid/liquid equilibrium for calcium (considering with Na, K) * precipitation of $\text{CaCO}_3, \text{Mg(OH)}_2$, Friedel's salt.	Absorption of Ca ions
CCT-P	$D(t) = D(0) \cdot \left(\frac{\phi(t)}{\phi(0)} \right)^n$	* Thermodynamic database * Incongruent dissolution of C-S-H * Dissolution/ precipitation of CaCO_3	Ion exchange reactions of Na, K, Ca and Mg

Simulation model

migration of Calcium ion



Boundary line (constant)

Diffusion coefficient(m²/s)

Composition of underground water (mmol/l)

Ca ²⁺	Na ⁺	K ⁺	Mg ²⁺	SO ₄ ²⁻	Cl ⁻	CO ₃ ²⁻	pH
0.13	0.77	0.03	0.16	0.14	0.44	0.62	8.6



Mix proportions of concrete and mortar

	W/B (%)	Air (%)	Unit Quantity (kg/m ³)					
			W	LPC	FA	LSP	S	G
Concrete	45	2.5	160	249	107	249	832	786
Mortar	45	2.5	230	358	153	307	1223	-

Cement hydrates using in calculation

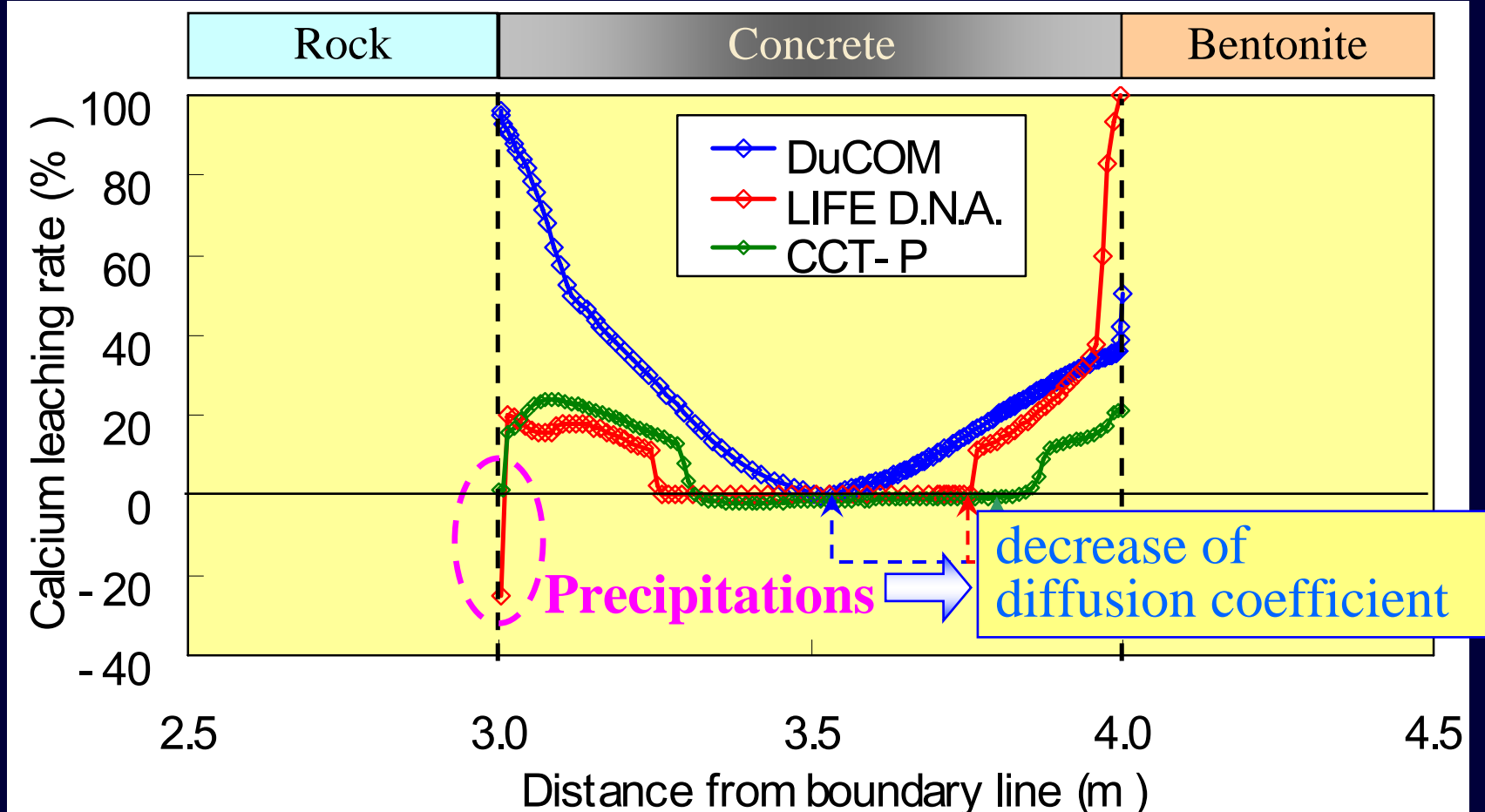
DuCOM ; Portlandite, C-S-H

LIFE D.N.A. ; Portlandite, C-S-H, Calcite, Brucite, Friedel's salt,
NaOH, KOH

CCT-P ; All hydrates in database

Simulation result of calcium leaching rate at 50,000 years

10



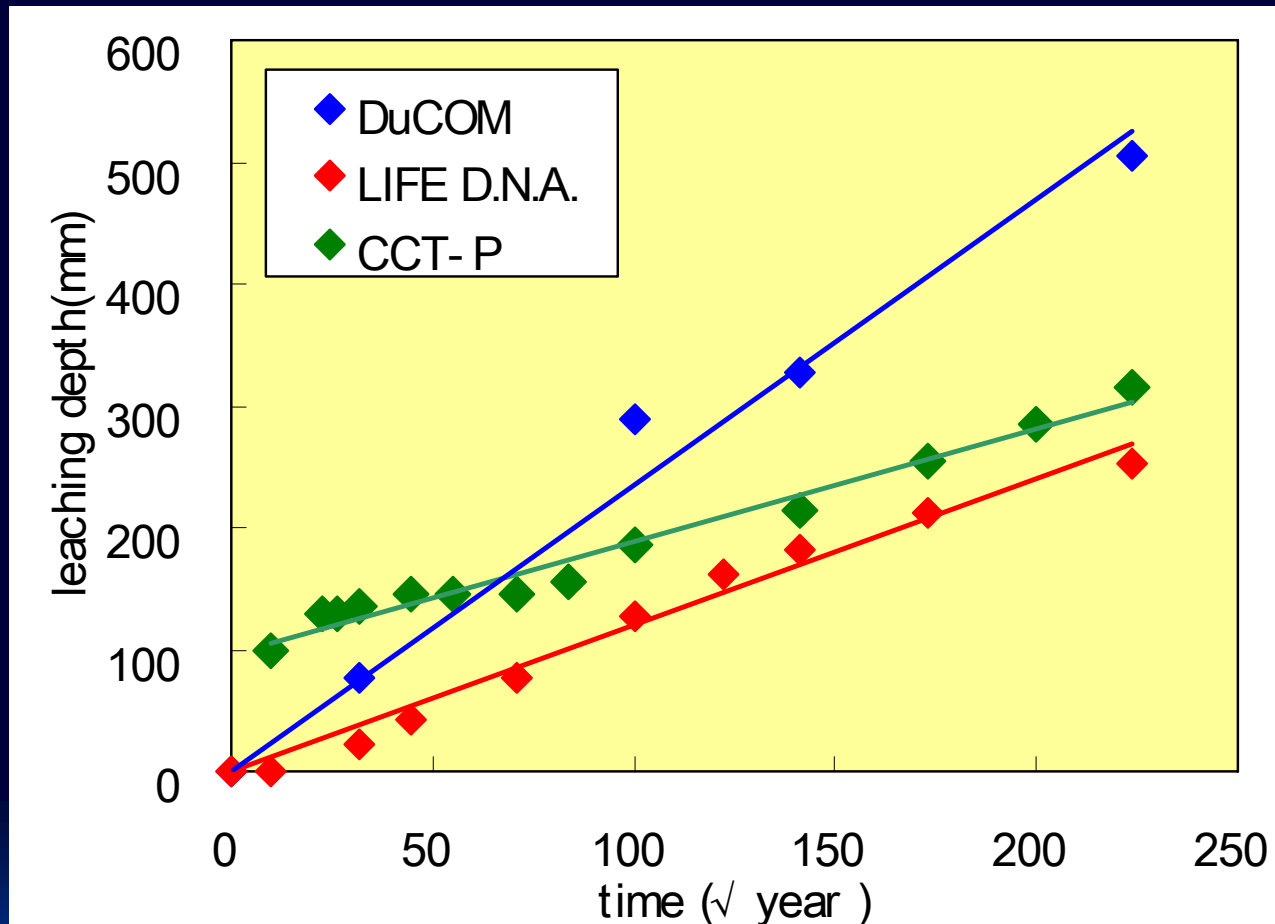
Faced to **Bentonite**

Leaching depth : DuCOM > LIFE D.N.A. > CCT-P

Faced to **Rock**

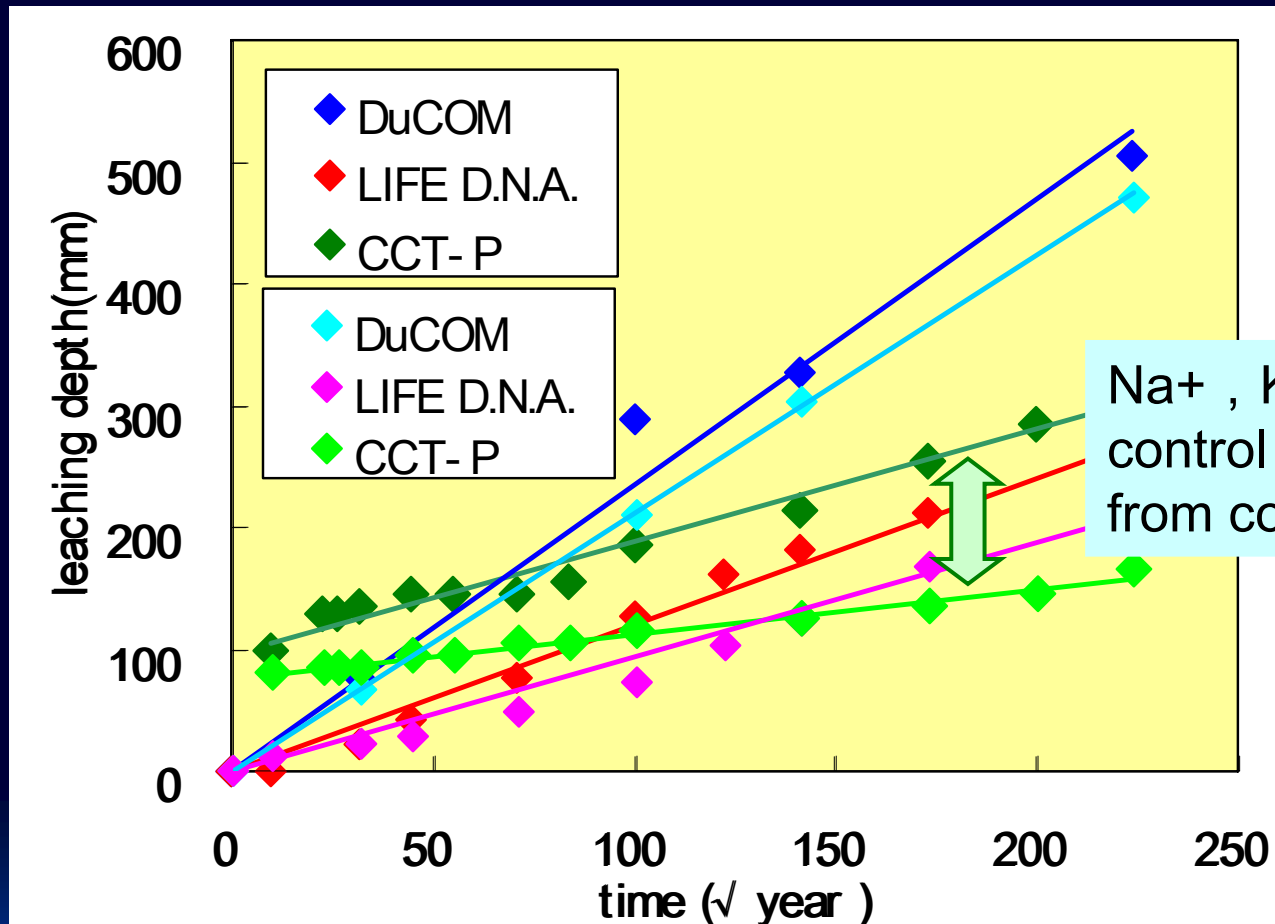
Leaching depth : DuCOM > CCT-P > LIFE D.N.A.

Calcium leaching speed of concrete (faced to rock)



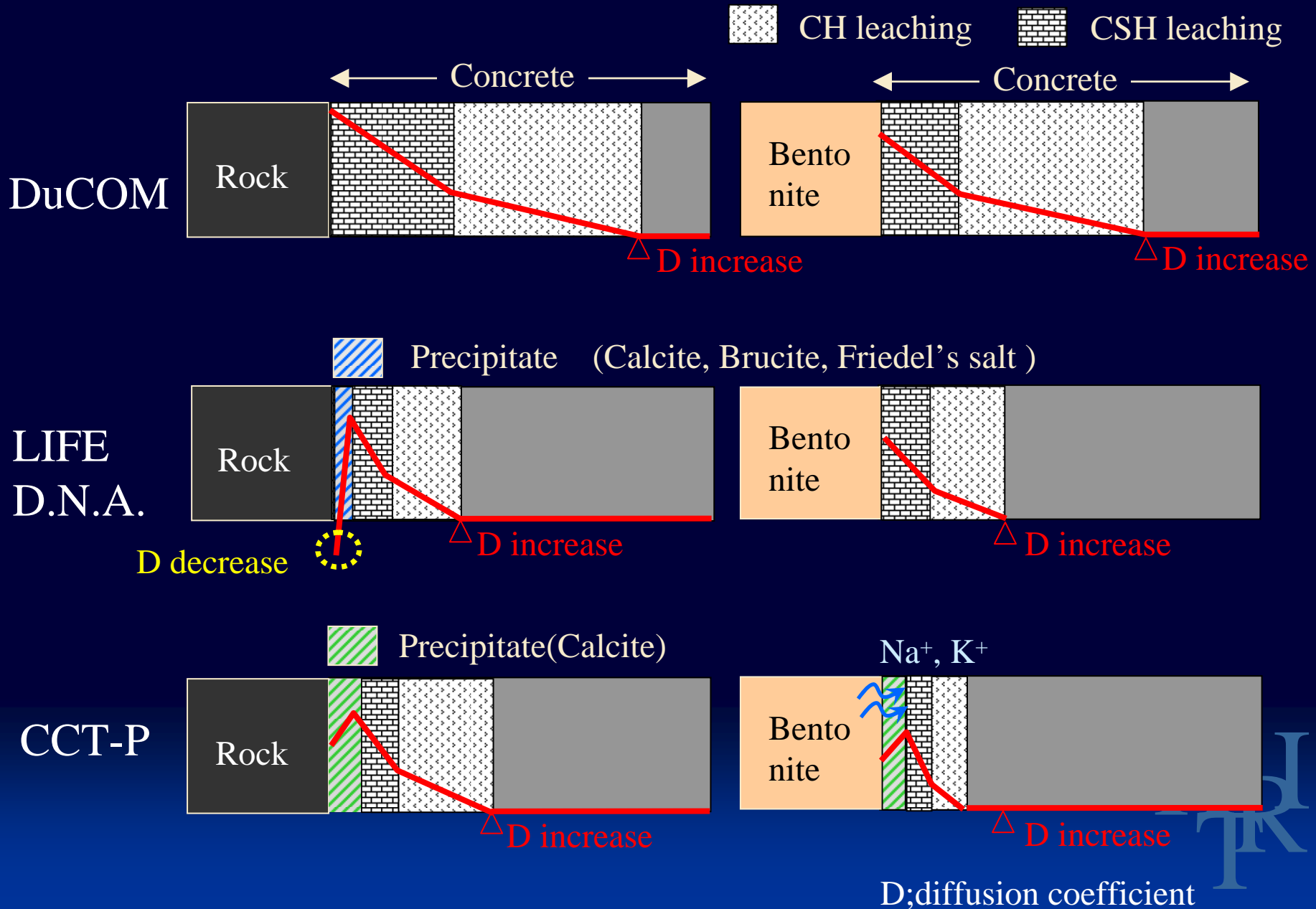
Leaching speed : DuCOM > LIFE D.N.A. > CCT-P

Calcium leaching speed of concrete (faced to rock & bentonite)



Na⁺ , K⁺ from Bentonite control Calcium leaching from concrete

Degradation process of cement hydrates



Dissolution/precipitation of cement hydrates

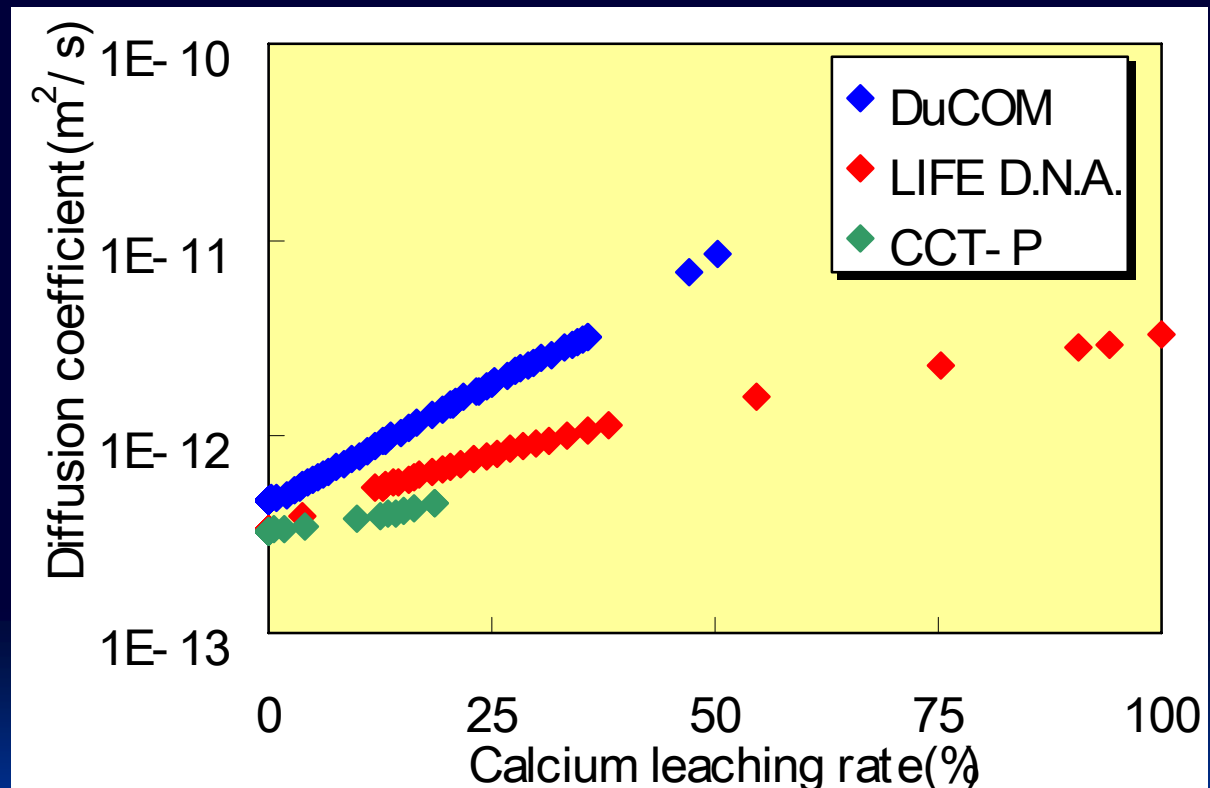
... Porosity increase/decrease

... Diffusion coefficient increase/decrease

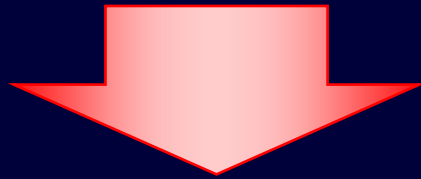
$$D_{eff} = \frac{\phi \cdot S}{\Omega} \cdot \delta \cdot D_{ion}$$

$$D_{eff}^i = \eta \cdot \beta \cdot f(\phi) \cdot D_0^i$$

$$D(t) = D(0) \cdot \left(\frac{\phi(t)}{\phi(0)} \right)^n$$



- Changing in diffusion coefficient
- Chemical reaction (especially, precipitation)



- Degradation process of cement hydrate is different
- Calcium leaching speed is different

Evaluating calcium leaching of cement hydrates by 3 codes.

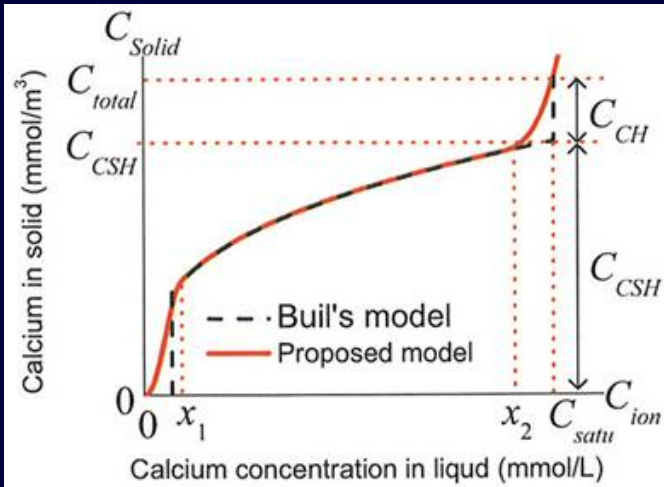
- What kind of deterioration will occur in sub-surface disposal repository?
 - Portlandite & C-S-H leach from cementitious material
 - Secondary minerals would precipitate
 - Degradation process is different in 3 codes
- How fast is the deterioration speed?
 - Calcium leaching speed is DuCOM > LIFE D.N.A. > CCT-P
 - Calcium leaching depth at 50,000 years are 130~500mm
 - The reason why simulation result is different...
 - Changing in diffusion coefficient
 - Chemical reaction (especially, precipitation)

Appendix



Dissolution/Precipitation of Hydrates

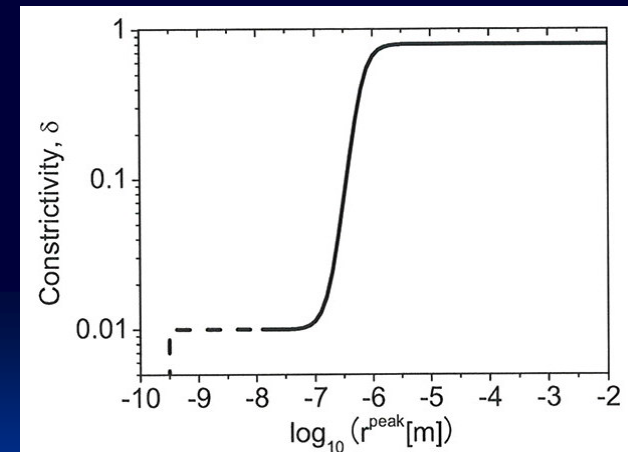
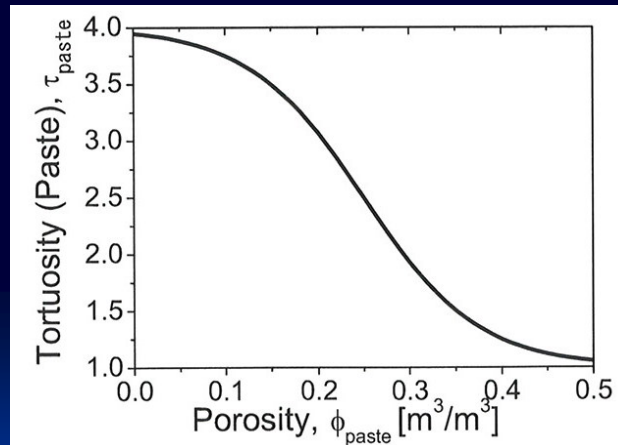
Calcium liquid/Solid equilibrium



Mass Transfer

- ◆ Transport by solution flow
- ◆ Transport by diffusion

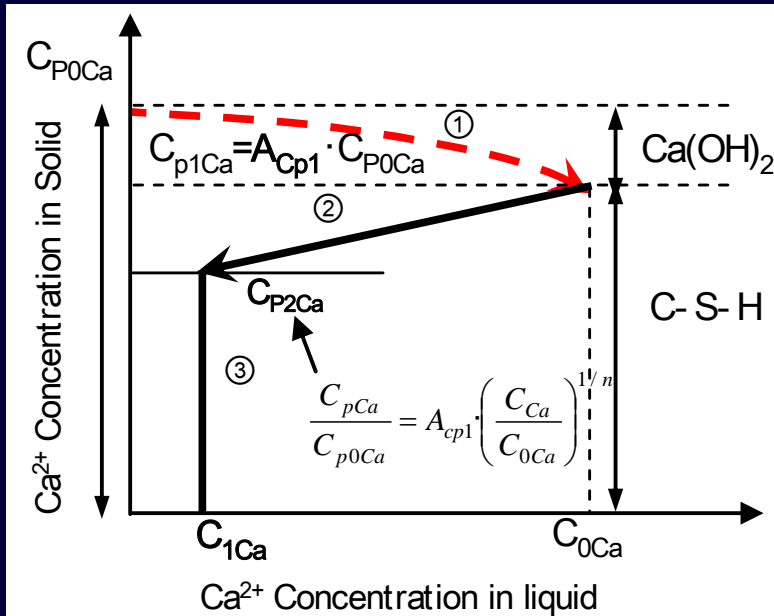
$$D_{eff} = \frac{\phi \cdot S}{\Omega} \cdot \delta \cdot D_{ion}$$



Calcium leaching = Porosity increase = D increase

Dissolution/Precipitation of Hydrates

Calcium liquid/Solid equilibrium



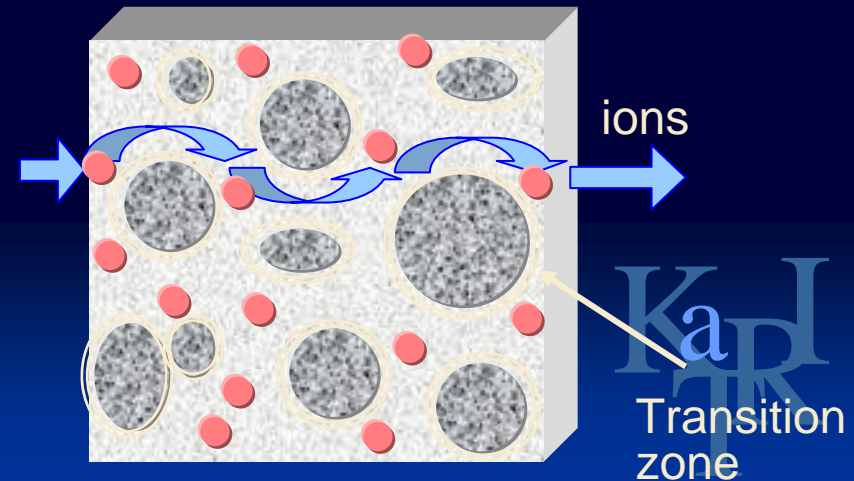
Mass Transfer

- ◆ Transport by solution flow
- ◆ Transport by diffusion
- ◆ Electric force

$$D_{eff}^i = \eta \cdot \beta \cdot f(\phi) \cdot D_0^i$$

$$f(\phi) = 0.001 + 0.07\phi^2 \{ 1.8(\phi - 0.18) \cdot H(\phi - 0.18) \}$$

$$\beta = \frac{1 - c \cdot G_{vol}}{1 - d \cdot S_{vol}} \cdot P_{vol}$$



Dissolution/Precipitation of Hydrates

◆ the thermodynamic database

(Chemical reaction code HARPHRQ)

◆ Incongruent dissolution of C-S-H

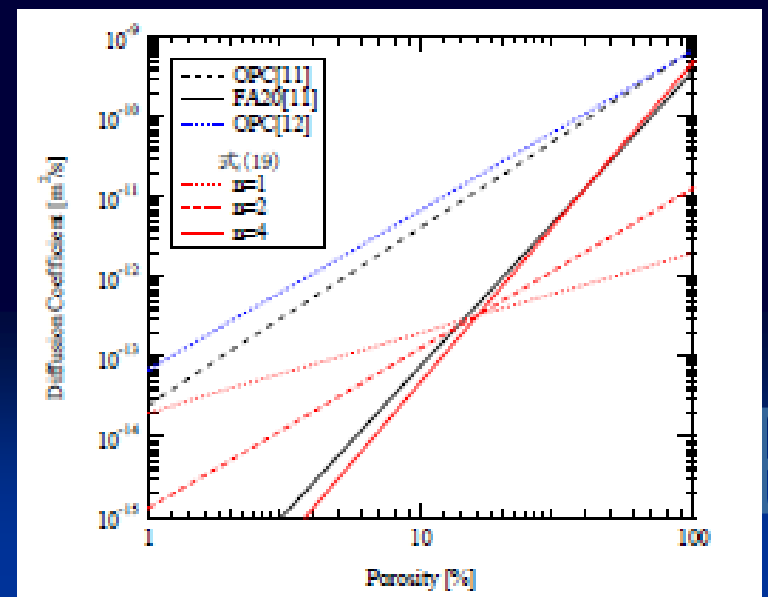
$$\log K_i = \frac{x^{i-1}}{1+x} \log K_{0i} - \frac{x^{i-1}}{1+x} \log\left(\frac{x^{i-1}}{1+x}\right) + \frac{x}{(1+x)^2} \left\{ A_{0i} + A_{1i} \frac{1-x}{1+x} + A_{2i} \left(\frac{1-x}{1+x}\right)^2 \right\}$$

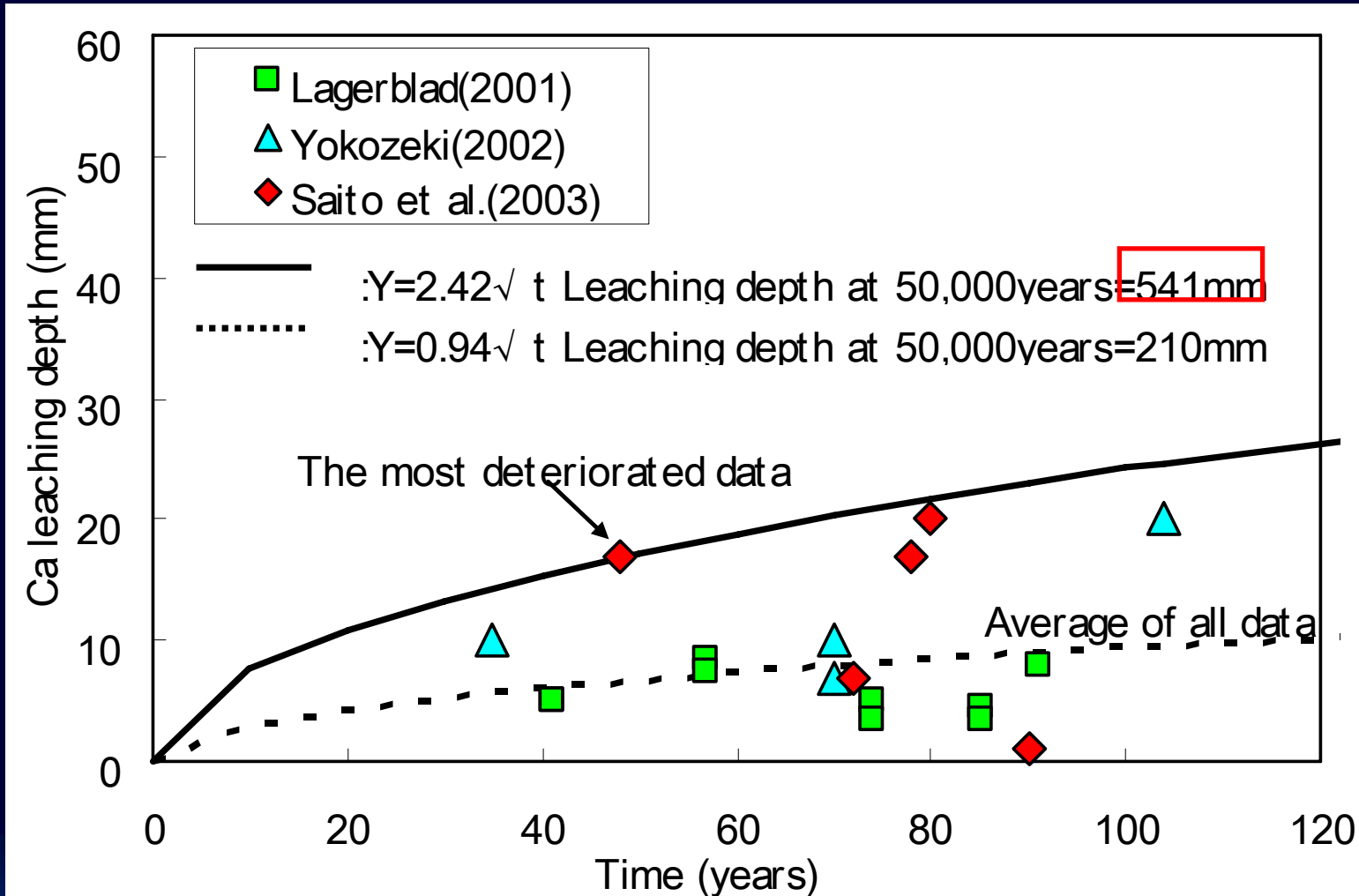
$\log K_{sp}$ of C-S-H gel depend on the rate of Ca/Si

Mass Transfer

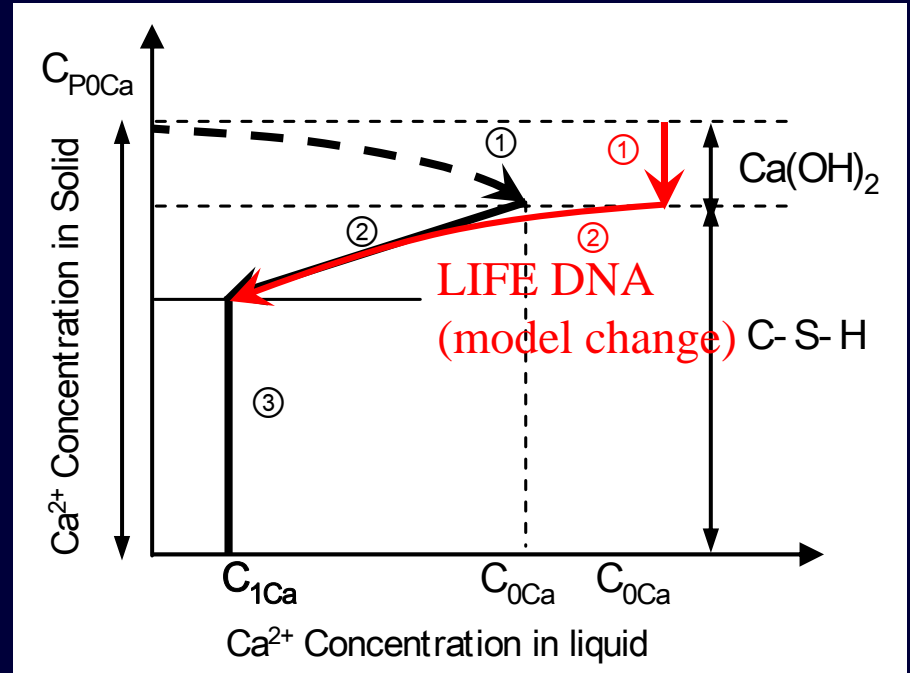
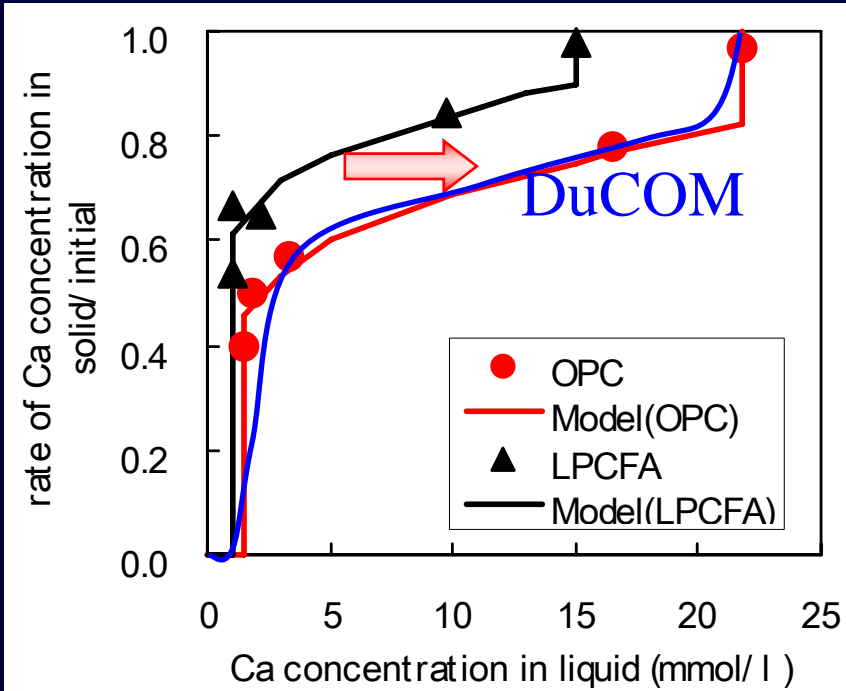
- ◆ Transport by solution flow
- ◆ Transport by diffusion

$$D(t) = D(0) \cdot \left(\frac{\phi(t)}{\phi(0)} \right)^n$$





Simulation results = 130 ~ 500mm at 50,000 years



<Different type of cements>

<effect Na ions & K ions>

